

RATINGS Limiting values in accordance with the Absolute Maximum System (IEC 134)

Collector-base voltage (open emitter)
peak value

V_{CBOM} max. 36 V

Collector-emitter voltage (open base)

V_{CEO} max. 18 V

Emitter-base voltage (open collector)

V_{EBO} max. 4 V

Collector current (average)

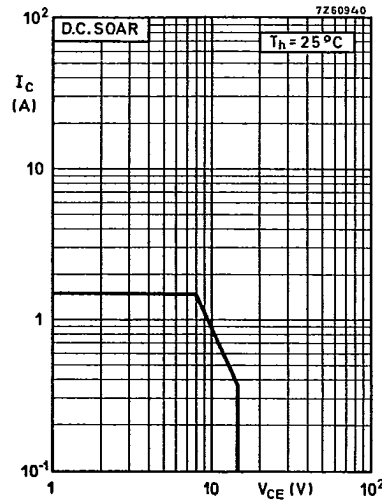
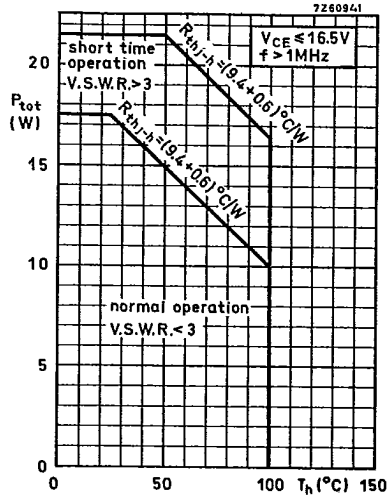
$I_{C(AV)}$ max. 1.25 A

Collector current (peak value) $f > 1$ MHz

I_{CM} max. 3.75 A

Total power dissipation up to $T_h = 25$ °C
 $f > 1$ MHz

P_{tot} max. 17.5 W



Storage temperature

T_{stg} -30 to +200 °C

Operating junction temperature

T_j max. 200 °C

THERMAL RESISTANCE

From junction to mounting base

$R_{th(j-mb)} = 9.4$ K/W

From mounting base to heatsink

$R_{th(mb-h)} = 0.6$ K/W

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April 1971

V.H.F. power transistor

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CHARACTERISTICS

$T_j = 25^\circ\text{C}$ unless otherwise specified

Collector cut-off current

$I_B = 0; V_{CE} = 14\text{ V}$ $I_{CEO} < 5\text{ mA}$

Breakdown voltages

Collector-base voltage
open emitter, $I_C = 1\text{ mA}$ $V_{(BR)CBO} > 36\text{ V}$

Collector-emitter voltage
open base, $I_C = 10\text{ mA}$ $V_{(BR)CEO} > 18\text{ V}$

Emitter-base voltage
open collector, $I_E = 1\text{ mA}$ $V_{(BR)EBO} > 4\text{ V}$

Transient energy

$L = 25\text{ mH}; f = 50\text{ Hz}$

open base $E > 0.5\text{ mS}$
 $-V_{BE} = 1.5\text{ V}; R_{BE} = 33\ \Omega$ $E > 0.5\text{ mS}$

D. C. current gain

$I_C = 500\text{ mA}; V_{CE} = 5\text{ V}$ $h_{FE} > 5$

Transition frequency

$I_C = 500\text{ mA}; V_{CE} = 10\text{ V}$ f_T typ. 700 MHz

Collector capacitance at $f = 1\text{ MHz}$

$I_E = I_e = 0; V_{CB} = 15\text{ V}$ C_c typ. 15 pF
< 20 pF

Feedback capacitance at $f = 1\text{ MHz}$

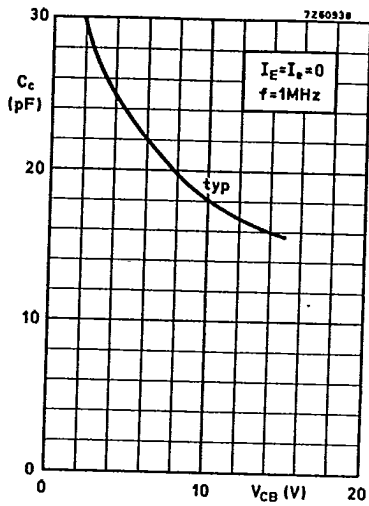
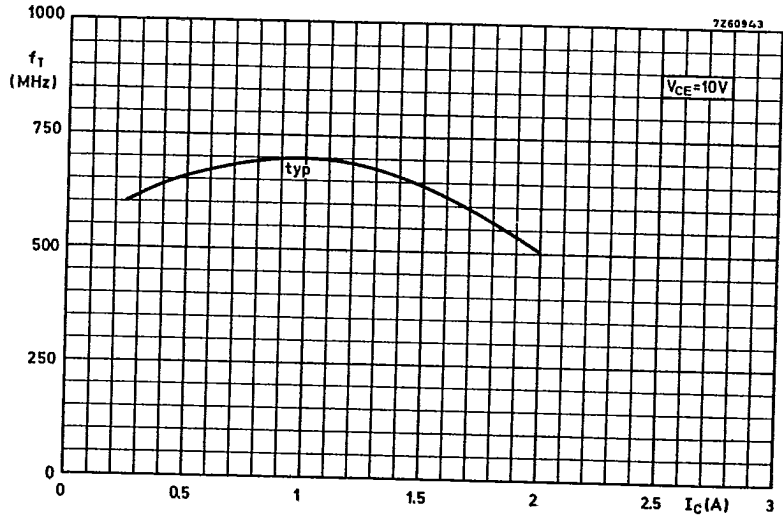
$I_C = 100\text{ mA}; V_{CE} = 15\text{ V}$ $-C_{re}$ typ. 11 pF

Collector-stud capacitance

C_{cs} typ. 2 pF

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NORTH/AMPEREX/DISCRETE 06E D



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V.H.F. power transistor

NORTH/AMPEREX/DISCRETE 06E D BLY87A

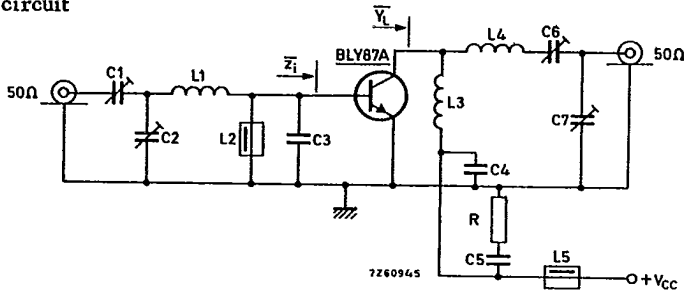
APPLICATION INFORMATION

R. F. performance in c. w. operation (unneutralised common-emitter class B circuit)

f = 175 MHz; T_{mb} up to 25°C

V _{CC} (V)	P _S (W)	P _L (W)	I _C (A)	G _p (dB)	η(%)	z _i (Ω)	Y _L (mS)
13.5	< 1.0	8	< 0.85	> 9	> 70	2.8 + j1.2	76 - j16
12.5	typ. 1.0	8	typ. 0.91	typ. 9	typ. 70	-	-

Test circuit



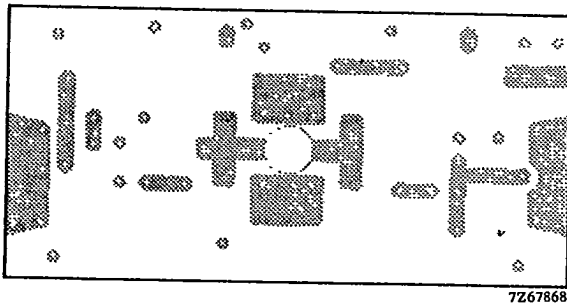
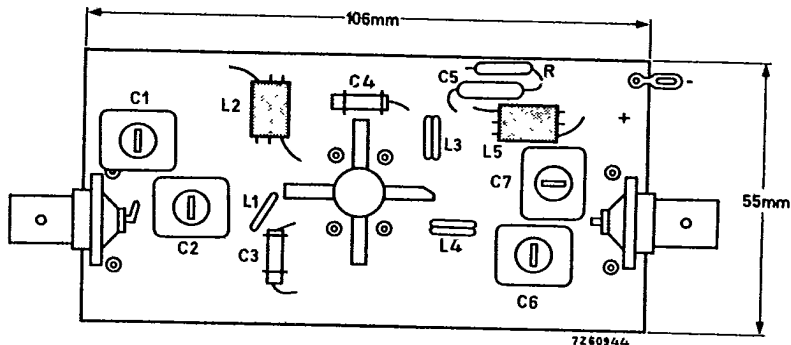
- C1 = 2.5 to 20 pF film dielectric trimmer (code number 2222 809 07004)
- C2 = C6 = C7 = 4 to 40 pF film dielectric trimmer (code number 2222 809 07008)
- C3 = 47 pF ceramic
- C4 = 100 pF ceramic
- C5 = 150 nF polyester
- L1 = 0.5 turn enamelled Cu wire (1.5 mm); int. diam. 6 mm; leads 2 x 10 mm
- L2 = L5 = ferroxcube choke (code number 4312 020 36640)
- L3 = 2.5 turns closely wound enamelled Cu wire (1.5 mm); int. diam. 6 mm; leads 2 x 10 mm
- L4 = 4.5 turns enamelled Cu wire (1.5 mm); int. diam. 6 mm; leads 2 x 10 mm
- R = 10 Ω carbon

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APPLICATION INFORMATION (continued)

Component lay-out and printed circuit board for 175 MHz test circuit.

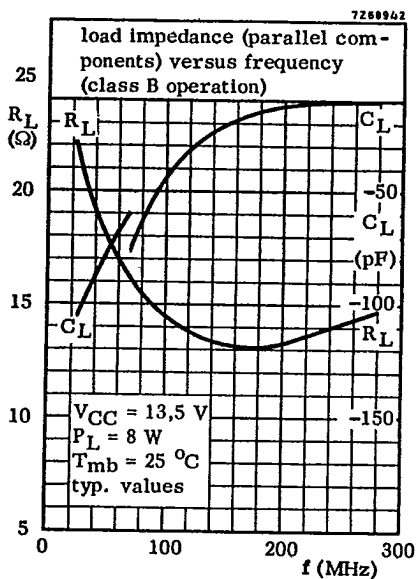
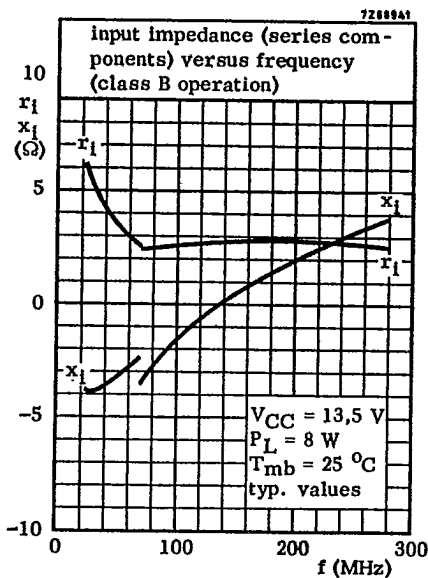
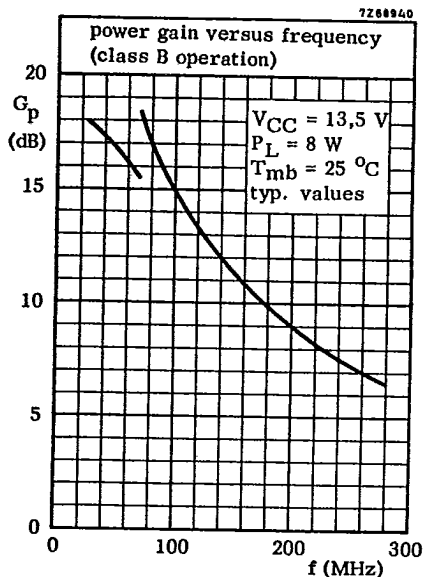
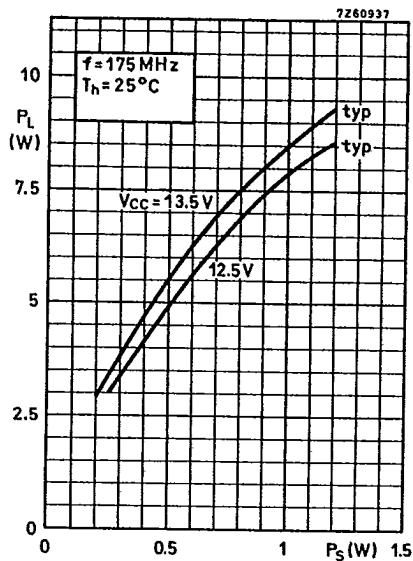


The circuit and the components are situated on one side of the epoxy fibre-glass board, the other side being fully metallised to serve as earth. Earth connections are made by means of hollow rivets.

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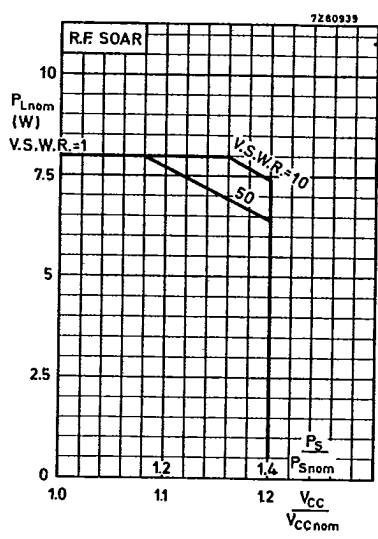
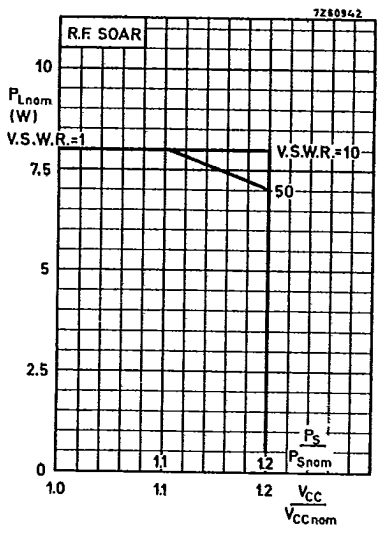
972 December 1973

OPERATING NOTE Below 70 MHz a base-emitter resistor of 10 Ω is recommended to avoid oscillation. This resistor must be effective for both d.c. and r.f.



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Conditions for R.F. SOAR:

f = 175 MHz $P_{Snom} = P_S$ at $V_{CC} = V_{CCnom}$ and V.S.W.R. = 1
 $T_h = 70^\circ C$ $R_{th mb-h} = 0.6 K/W$
 $V_{CCnom} = 12.5$ or $13.5 V$

The transistor has been developed for use with unstabilized supply voltages. As the output power and drive power increase with the supply voltage, the nominal output power must be derated in accordance with the graphs above for safe operation at supply voltages other than the nominal. The graphs show the allowable output power under nominal conditions, as a function of the supply overvoltage ratio, with V. S. W. R. as parameter.

The left hand graph applies to the situation in which the drive (P_S/P_{Snom}) increases linearly with supply overvoltage ratio.

The right hand graph shows the derating factor to be applied when the drive (P_S/P_{Snom}) increases as the square of the supply overvoltage ratio (V_{CC}/V_{CCnom}).

Depending on the operating conditions, the appropriate derating factor may lie in the region between the linear and the square-law functions.

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974 April 1971